



A Product Line of Diodes Incorporated



# ZXGD3105N8

### SYNCHRONOUS MOSFET CONTROLLER IN SO-8

### Description

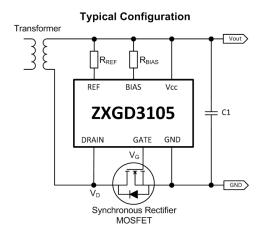
ZXGD3105N8 synchronous controller is designed for driving a MOSFET as an ideal rectifier. This is to replace a diode for increasing the power transfer efficiency.

The device is comprised of a differential amplifier detector stage and high current driver. The detector monitors the reverse voltage of the MOSFET such that if body diode conduction occurs a positive voltage is applied to the MOSFET's Gate pin. Once the positive voltage is applied to the Gate the MOSFET switches on allowing reverse current flow. The detectors' output voltage is then proportional to the MOSFET Drain-Source voltage and this is applied to the Gate via the driver. This action provides a rapid MOSFET turn off as Drain current decays to zero.

### Applications

Flyback and Resonant Converters in:

- Low Voltage AC / DC Adaptors
- Set Top Box
- Computing Power Supplies ATX and Server PSU
- Low Voltage DC / DC conversion



# Ordering Information (Note 3)

Product	Marking	Reel size (inches)	Tape width (mm)	Quantity per reel
ZXGD3105N8TC	ZXGD 3105	13	12	2500

Notes: 1. No purposefully added lead

2. Diodes Inc's "Green" Policy can be found on our website at http://www.diodes.com

3. For packaging details, go to our website at http://www.diodes.com

# Marking Information

ZXGD							
3105 YY WW							
•	•••						

ZXGD = Product Type Marking Code, Line 1 3105

= Product Type Marking Code, Line 2

= Year (ex: 11 = 2011)

= Week (01 - 53)

YΥ

WW

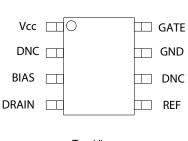
### Features

- Low standby power with quiescent supply current < 1mA •
- 4.5V operation enables low voltage supply
- Proportional gate drive for fast turn-off
- Operation up to 500kHz
- Critical Conduction Mode (CrCM) & Continuous Mode (CCM)
- Compliant with Eco-design directive
- "Lead-Free", RoHS Compliant (Note 1)
- Halogen and Antimony free. "Green" Device (Note 2)
- Qualified to AEC-Q101 Standards for High Reliability

### **Mechanical Data**

- Case: SO-8
- Case material: Molded Plastic. "Green" Molding Compound.
- UL Flammability Rating 94V-0
- Moisture Sensitivity: Level 1 per J-STD-020
- Terminals: Matte Tin Finish
- Solderable per MIL-STD-202, Method 208
- Weight: 0.074 grams (approximate)

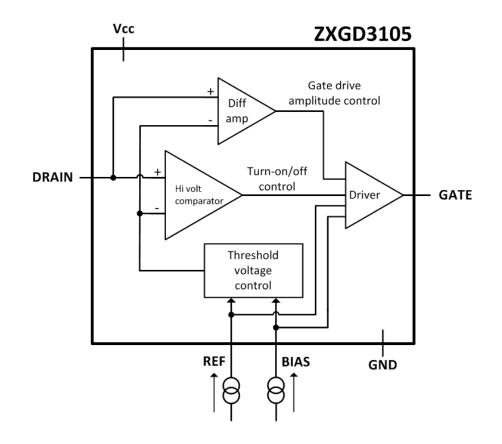
**SO-8** 



Top View Pin-Out



# **Functional Block Diagram**



Pin #	Pin Name	Pin Function and Description
1	Vcc	<b>Power supply</b> This supply pin should be closely decoupled to ground with a ceramic capacitor.
2	DNC	<b>Do not connect</b> Leave pin floating.
3	BIAS	<b>Bias</b> Connect this pin to Vcc via R <sub>BIAS</sub> resistor. Select R <sub>BIAS</sub> to source 0.54mA into this pin. Refer to Table 1 and 2, in Application Information section.
4	DRAIN	<b>Drain sense</b> Connect directly to the synchronous MOSFET drain terminal.
5	REF	<b>Reference</b> Connect this pin to Vcc via $R_{REF}$ resistor. Select $R_{REF}$ to source 1.02mA into this pin. Refer to Table 1 and 2, in Application Information section.
6	DNC	Do not connect Leave pin floating.
7	GND	Ground Connect this pin to the synchronous MOSFET source terminal and ground reference point.
8	GATE	Gate drive This pin sinks and sources the $I_{SINK}$ and $I_{SOURCE}$ current to the synchronous MOSFET gate.



### Maximum Ratings @T<sub>A</sub> = 25°C unless otherwise specified

Characteristic	Symbol	Value	Unit
Supply voltage, relative to GND	Vcc	15	V
Drain pin voltage	V <sub>D</sub>	-3 to 100	V
Gate output voltage	V <sub>G</sub>	-3 to V <sub>CC</sub> + 3	V
Gate Driver peak source current	ISOURCE	4	A
Gate Driver peak sink current	I <sub>SINK</sub>	9	A
Reference voltage	V <sub>REF</sub>	V <sub>CC</sub>	V
Reference current	I <sub>REF</sub>	25	mA
Bias voltage	V <sub>BIAS</sub>	V <sub>CC</sub>	V
Bias current	I <sub>BIAS</sub>	100	mA

# Thermal Characteristics $@T_A = 25^{\circ}C$ unless otherwise specified

Characteristic	Characteristic			Unit	
	(Note 4)		490 3.92		
Power Dissipation	(Note 5)		655 5.24	mW	
Linear derating factor	(Note 6)	P <sub>D</sub>	720 5.76	mW/°C	
	(Note 7)		785 6.28		
	(Note 4)		255		
Thermal Desistance, lunction to Ambient	(Note 5)		191	0000	
Thermal Resistance, Junction to Ambient	(Note 6)	R <sub>0JA</sub>	173	°C/W	
	(Note 7)		159		
Thermal Resistance, Junction to Lead	(Note 8)	R <sub>θJL</sub>	135	°C/W	
Operating Temperature Range	TJ	-40 to +150			
Storage Temperature Range		T <sub>STG</sub>	-50 to +150		

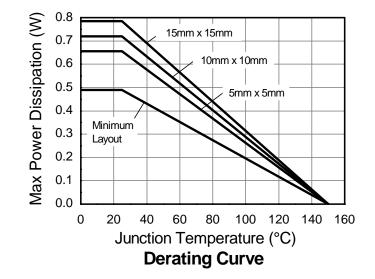
4. For a device surface mounted on minimum recommended pad layout FR4 PCB with high coverage of single sided 1oz copper, in still air conditions; the Notes: device is measured when operating in a steady-state condition. 5. Same as note (4), except pin 1 ( $V_{cc}$ ) and pin 7 (GND) are both connected to separate 5mm x 5mm 1oz copper heatsinks. 6. Same as note (5), except both heatsinks are 10mm.

7. Same as note (5), except both heatsinks are 15mm x 15mm.

8. Thermal resistance from junction to solder-point at the end of each lead on pin 1 (V<sub>CC</sub>) and pin 7 (GND).



# **Thermal Derating Curve**



# **ESD** Rating

Characteristic	Value	Unit
ESD for Human Body Model	4000	V
ESD for Machine Model	200	v



EX

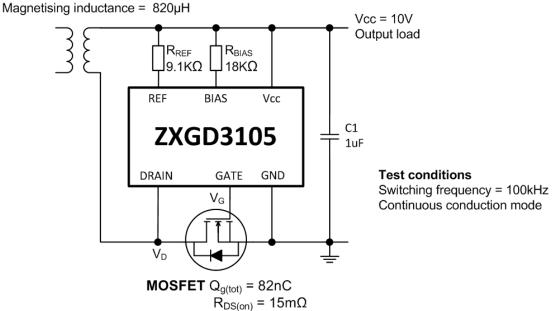
### Electrical Characteristics @T<sub>A</sub> = 25°C unless otherwise specified

#### $V_{CC} = 10V$ ; $R_{BIAS} = 18k\Omega$ ( $I_{BIAS} = 0.54mA$ ); $R_{REF} = 9.1k\Omega$ ( $I_{REF} = 1.02mA$ )

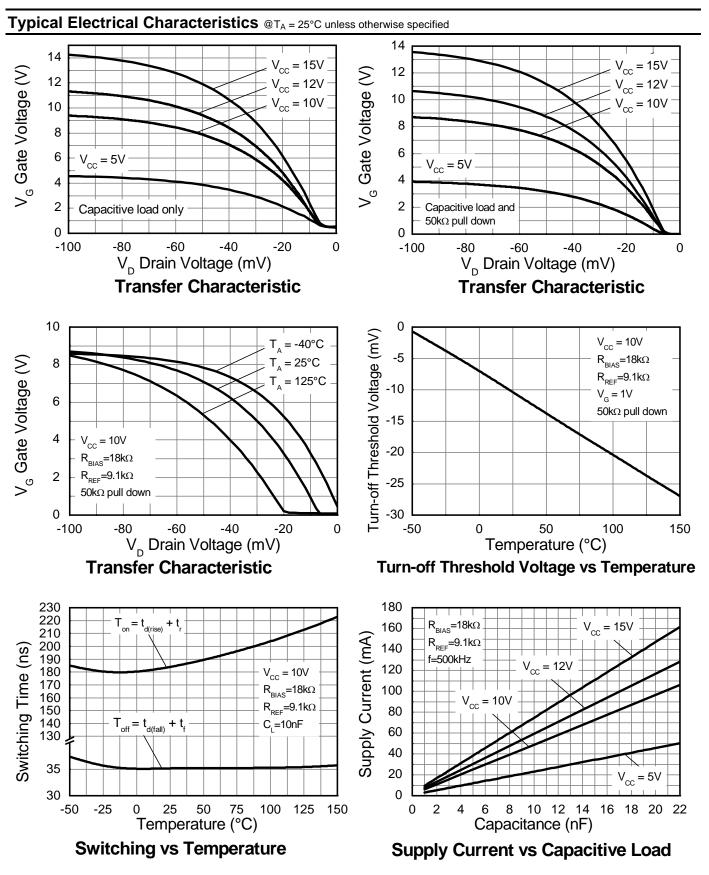
Characteristic	Symbol	Min	Тур	Max	Unit	Test Condition		
Input Supply								
Quiescent current	lq	-	1.56	-	mA	V <sub>DRAIN</sub> ≥ 0mV		
Gate Driver								
Gate peak source current	ISOURCE	-	2	-	А	Capacitive load: $C_L = 20nF$		
Gate peak sink current	I <sub>SINK</sub>	-	7	-	A			
Detector under DC condition								
Turn-off Threshold Voltage	VT	-20	-10	0	mV	$V_{G} = 1V$		
	V <sub>G(off)</sub>	-	0.2	0.6		V <sub>DRAIN</sub> ≥1V	Capacitive load only	
Gate output voltage		5.0	7.8		V	$V_{DRAIN} = -50mV$		
	V <sub>G</sub>	8.0	9.4			$V_{DRAIN} = -100 mV$	1	
Switching Performance								
Turn-on propagation delay	t <sub>d(rise)</sub>	-	70	-				
Gate rise time	tr	-	175	-	<b></b>	Rise and fall measured 10% to 90% Refer to application test circuit below		
Turn-off propagation delay	t <sub>d(fall)</sub>	-	15	-	ns			
Gate fall time	t <sub>f</sub>	-	20	-	1			

# **Test Circuit for Switching Performance**

### Flyback transformer

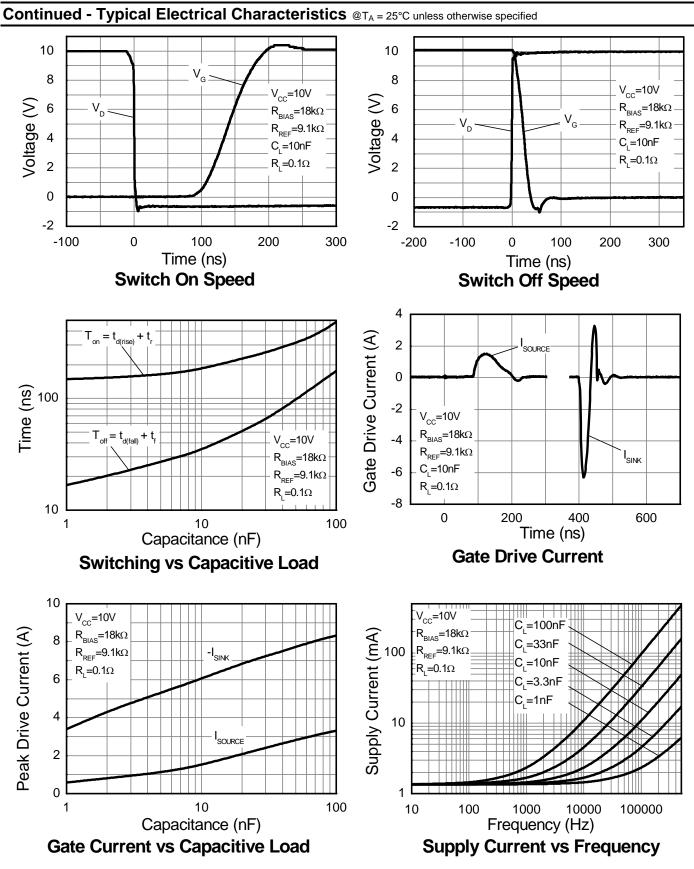






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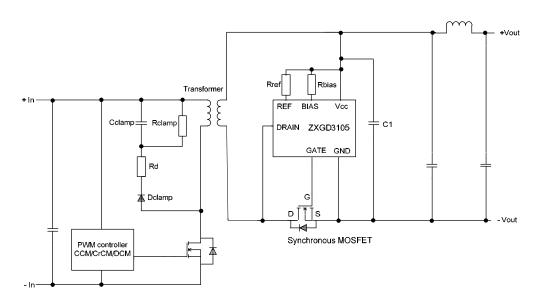


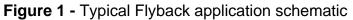
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# **Application Information**

The purpose of the ZXGD3105 is to drive a MOSFET as a low-V<sub>F</sub> Schottky diode replacement in isolated AC/DC converter. When combined with a low  $R_{DS(ON)}$  MOSFET, the controller can yield significant power efficiency improvement, whilst maintaining design simplicity and incurring minimal component count. Figure 1 shows the typical configuration of ZXGD3105 for synchronous rectification in a low output voltage Flyback converter.





# Threshold voltage and resistor setting

Proper selection of external resistors  $R_{REF}$  and  $R_{BIAS}$  is important for optimum device operation.  $R_{REF}$  and  $R_{BIAS}$  supply fixed current into the  $I_{REF}$  and  $I_{BIAS}$  pin of the controller.  $I_{REF}$  and  $I_{BIAS}$  combines to set the turn-off threshold voltage level,  $V_T$ . In order to set  $V_T$  to -10mV, the recommended  $I_{REF}$  and  $I_{BIAS}$  are 1.02mA and 0.54mA respectively.

The values for  $R_{REF}$  and  $R_{BIAS}$  are selected based on the Vcc voltage. If the Vcc pin is connected to the power converter's output, the resistors should be selected based on the nominal converter's output voltage. Table 1 provides the recommended resistor values for different Vcc voltages.

Supply, Vcc	Bias Resistor, R <sub>BIAS</sub>	Reference Resistor, $R_{REF}$		
5 V	9.6 kΩ	4.3 kΩ		
10 V	18 kΩ	9.1 kΩ		
12 V	24 kΩ	11 kΩ		
15 V	30 kΩ	15 kΩ		

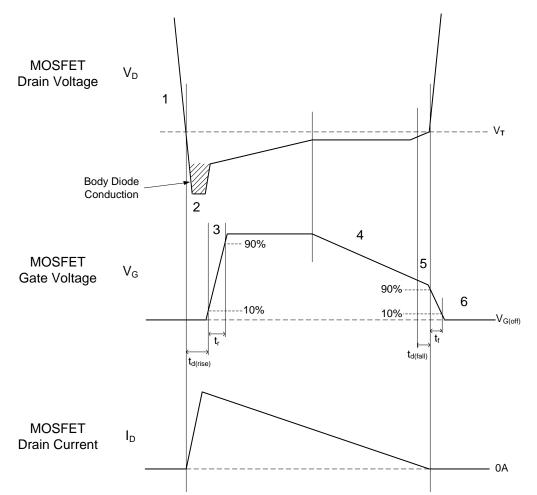
 Table 1 – Recommended resistor values for different Vcc voltages



# **Functional descriptions**

The operation of the device is described step-by-step with reference to the timing diagram in Figure 2.

- 1. The detector stage monitors the MOSFET Drain-Source voltage.
- 2. When, due to transformer action, the MOSFET body diode is forced to conduct there is a negative voltage on the Drain pin due to the body diode forward voltage.
- 3. When the negative Drain voltage crosses the turn-off Threshold voltage V<sub>T</sub>, the detector stage outputs a positive voltage with respect to ground after the turn-on delay time  $t_{d(fall)}$ . This voltage is then fed to the MOSFET driver stage and current is sourced out of the GATE pin.
- 4. The controller goes into proportional gate drive control the GATE output voltage is proportional to the MOSFET on-resistance-induced Drain-Source voltage. Proportional gate drive ensures that MOSFET conducts during majority of the conduction cycle to minimize power loss in the body diode.
- 5. As the Drain current decays linearly toward zero, proportional gate drive control reduces the Gate voltage so the MOSFET can be turned off rapidly at zero current crossing. The GATE voltage falls to 1V when the Drain-Source voltage crosses the detection threshold voltage to minimize reverse current flow.
- 6. At zero Drain current, the controller GATE output voltage is pulled low to  $V_{G(off)}$  to ensure that the MOSFET is off.





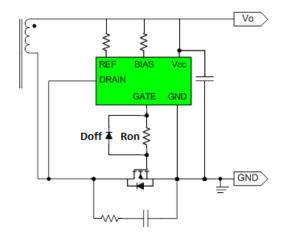




# Gate driver

The controller is provided with single channel high current gate drive output, capable of driving one or more Nchannel power MOSFETs. The controller can operate from Vcc of 4.5V to drive both standard MOSFETs and logic level MOSFETs.

The Gate pins should be as close to the MOSFET's gate as possible. A resistor in series with GATE pin helps to control the rise time and decrease switching losses due to gate voltage oscillation. A diode in parallel to the resistor is typically used to maintain fast discharge of the MOSFET's gate.





# Quiescent current consumption

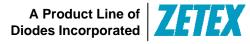
The quiescent current consumption of the controller is the sum of  $I_{REF}$  and  $I_{BIAS}$ . For an application that requires ultralow standby power consumption,  $I_{REF}$  and  $I_{BIAS}$  can be further reduced by increasing the value of resistor  $R_{REF}$  and  $R_{BIAS}$ .

Bias Current I <sub>BIAS</sub>	Ref Current I <sub>REF</sub>	Bias Resistor R <sub>BIAS</sub>	Ref Resistor R <sub>REF</sub>	Quiescent Current I <sub>Q</sub>
0.25mA	0.61mA	39.2KΩ	15.4KΩ	0.86mA
0.35mA	0.81mA	28.0KΩ	11.5KΩ	1.16mA
0.46mA	0.99mA	21.5KΩ	9.3KΩ	1.45mA
0.50mA	1.00mA	19.6KΩ	8.9KΩ	1.50mA
0.55mA	1.13mA	17.8KΩ	8.1KΩ	1.68mA
0.80mA	1.66mA	12.1KΩ	5.6KΩ	2.46mA

 Table 2 – Quiescent current consumption for different resistor values at Vcc=10V

 $I_{REF}$  also controls the gate driver peak sink current whilst  $I_{BIAS}$  controls the peak source current. At the default current value of  $I_{REF}$  and  $I_{BIAS}$  of 1.02mA and 0.54mA, the gate driver is able to provide 2A source and 6A sink current. The gate current decreases if  $I_{REF}$  and  $I_{BIAS}$  are reduced. Care must be taken in reducing the controller quiescent current so that sufficient drive current is still delivered to the MOSFET particularly for high switching frequency application.





# Layout guidelines

When laying out the PCB, care must be taken in decoupling the ZXGD3105 closely to  $V_{CC}$  and ground with 1µF low-ESR, low-ESL X7R type ceramic bypass capacitor. If the converter's output voltage is higher than 15V, a series voltage regulator between the converter's output voltage and the Vcc pin, can be used to get a stable Vcc voltage.

GND is the ground reference for the internal high voltage amplifier as well as the current return for the gate driver. So the ground return loop should be as short as possible. Sufficient PCB copper area should be allocated to the Vcc and GND pin for heat dissipation especially for high switching frequency application.

Any stray inductance involved by the load current may cause distortion of the drain-to-source voltage waveform, leading to premature turn-off of the synchronous MOSFET. In order to avoid this issue, drain voltage sensing should be done as physically close to the drain terminals as possible. The PCB track length between the controller Drain pin and MOSFET's terminal should be kept less than 10mm. MOSFET packages with low internal wire bond inductance are preferred for high switching frequency power conversion to minimize body diode conduction.

After the primary MOSFET turns off, its drain voltage oscillates due to reverse recovery of the snubber diode. These high frequency oscillations are reflected across the transformer to the drain terminal of the synchronous MOSFET. The synchronous controller senses the drain voltage ringing, causing its gate output voltage to oscillate. The synchronous MOSFET cannot be fully enhanced until the drain voltage stabilizes.

In order to prevent this issue, the oscillations on the primary MOSFET can be damped with either a series resistor Rd to the snubber diode or an R-C network across the diode. Both methods reduce the oscillations by softening the snubber diode's reverse recovery characteristic.

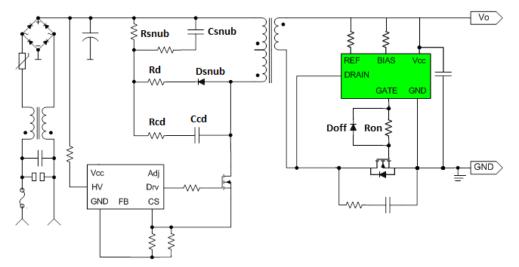
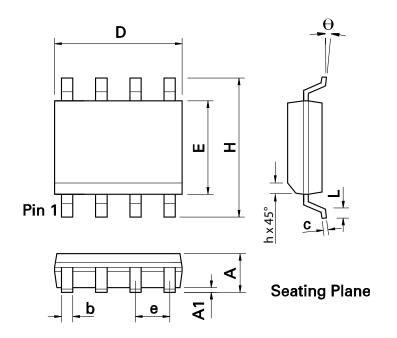


Figure 4 - Primary side snubber network to reduce drain voltage oscillations



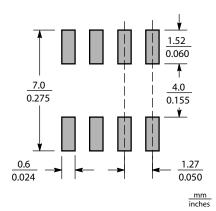
ΕX

# **Package Outline Dimensions**



DIM	Inc	hes	Millimeters		DIM	Inches		Millimeters	
	Min.	Max.	Min.	Max.		Min.	Max.	Min.	Max.
А	0.053	0.069	1.35	1.75	е	0.050 BSC		1.27 BSC	
A1	0.004	0.010	0.10	0.25	b	0.013	0.020	0.33	0.51
D	0.189	0.197	4.80	5.00	С	0.008	0.010	0.19	0.25
н	0.228	0.244	5.80	6.20	θ	0°	8°	0°	8°
E	0.150	0.157	3.80	4.00	h	0.010	0.020	0.25	0.50
L	0.016	0.050	0.40	1.27	-	-	-	-	-

# **Suggested Pad Layout**





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